

RESONATOR CAVITY CONFIGURATION AND METHOD

FIELD OF THE INVENTION

This invention relates to a resonator cavity configuration and a method of laser beam generation.

5 LIST OF REFERENCES

The following references are considered to be pertinent for the purpose of understanding the background of the present invention:

- [1] M. Jr. DiDomenico, "A single-frequency TEM₀₀ - mode gas laser with high output power", Appl Phys. Lett. 8, no. 1, 20-22 (1966).
- 10 [2] M. Jr. DiDomenico, "Characteristics of a single-frequency Michelson-type He-Ne gas laser", IEEE JQE QE-2, no. 8, 311-322 (1966).
- [3] M. Brunel, A. Le Floch and F. Bretenaker, "Multiaxis laser eigenstates", J. opt. Soc. Am. B 13, 946-960 (1996).
- [4] J. R. Leger, G. J. Swanson and W. B. Veldkamp, "Coherent addition
15 using binary phase gratings", Applied Optics 26, 4391-4399 (1987).
- [5] T. S. Rutherford and R. L. Byer, "Six beam phase-locked slab laser resonator", CLEO/Europe-EQEC, the 15th international conference on lasers and electrooptics, Munich Germany (2001).
- [6] S. Menard, M. Vampouille, A. Desfarges-Berthelemot, V. Kermene,
20 B. Colombeau and C. Froehly, "Highly efficient phase locking of four diode pumped Nd:YAG laser beams", Opt. Comm. 160, 344-353 (1999).
- [7] D. Sabourdy, V. Kermene, A. Desfarges-Berthelemot, M. Vampouille and A. Barthelemy, "Coherent combining of two Nd:YAG lasers in a Vernier-Michelson-type cavity", Appl. Phys. B 75, 503-507 (2002).
- 25 [8] V. A. Kozlov, J. Hernandez-Cordero and T. F. Morse, "All-fiber coherent beam combining of fiber lasers", Opt Lett. 24, 1814-1816 (1999).

- [9] D. Sabourdy, V. Kermene, A. Desfarges-Berthelemot, L. Lefort and A. Barthelemy, C. Mahodaux and D. Pureur, "Power scaling of fiber lasers with all-fiber interferometric cavity", *Electronics Letters* 38, no. 14, 692-693 (2002).
- [10] A. Shirakawa, T. Saitou, T. Sekiguchi and K. Ueda, "Coherent
5 addition of fiber lasers by use of a fiber coupler", *Optics Express* 10, no. 21, 1167-1172 (2002).
- [11] D. Sabourdy, V. Kermene, A. Desfarges-Berthelemot, L. Lefort and A. Barthelemy, "Efficient coherent combining of widely tunable fiber lasers", *Optics Express* 11, vol. 2, 87-97 (2003).
- 10 [12] G. Machavariani, N. Davidson, A. Ishaaya, E. Hasman, and A. A. Friesem, "Efficient formation of high-quality beam from a pure high order Hermite-Gaussian mode", *Opt. Lett.* 27, 1501-1503 (2002).
- [13] A. A. Ishaaya, G. Machavariani, N. Davidson, E. Hasman and A. A. Friesem, "Conversion of a high-order mode beam into a nearly Gaussian Beam
15 using a single interferometric element", *Opt. Lett.* 28, 504-506 (2003);
- [14] Oron et al., *Progress in Optics*, vol. 42, pp. 325-385, 2001.

BACKGROUND OF THE INVENTION

High-power lasers are typically characterized by inferior beam quality,
20 stability, and heat dissipation, as compared to that of lower power lasers. Combining several low-power lasers by incoherently adding the field distributions of several laser output beams results in that the combined beam-quality factor (M^2) is relatively poor with low optical brightness. When the field distributions are coherently added, with the proper phase relations, the combined beam quality factor
25 can be as good as that of one low-power laser, while the combined power is greater by a factor equal to the number of the lasers.

When coherently combining two or more laser output fields, two major difficulties are encountered. The first results from the need for proper coupling between the individual laser fields, so as to enable relative phase locking between
30 them. Such coupling typically introduces excessive losses to each laser field, and requires very accurate relative alignment. The second (and somewhat related)

difficulty results from the need for accurately controlling the relative phase between the different laser fields, so as to ensure constructive interference between them. This requires that the distances between the participating optical components must be very accurately controlled, causing the output power to be extremely sensitive to thermal drifts and acoustic vibrations.

Attempts have been made to obtain high power concomitantly with good beam quality based on intra-cavity phase locking and coherent addition of lasers [1-7]. Several techniques dealing with intra-cavity coherent addition of single transverse mode (TEM_{00}) laser beams in fiber lasers have been developed [8-11]. According to these techniques, the phase locking and coherent addition is accomplished by the use of fiber couplers. Single transverse mode fiber couplers (2x2 for example) have been used recently to obtain intra-cavity coherent addition of single transverse mode (TEM_{00}) laser beams in a fiber laser configuration [8-11]. Here, one of the output terminals of the 2x2 standard single mode fiber coupler was angle spliced so that no reflection from that terminal is present. The resulting coupler's operation when placed in a resonator is similar to that of a 50% beam splitter. This approach, however, is applicable only in fiber laser systems, and designed only for single TEM_{00} beams.

U.S. Patent No. 3,414,840 discloses a technique of synchronization of power sources. Here, two laser oscillators are used, each including a first mirror and a laser medium and each sharing in common a second mirror, and means for extracting wave energy from the oscillators. The first mirrors and the common second mirror form a pair of resonant cavities. A 3db hybrid junction, having two pairs of conjugate ports located within a common region of the cavities, is used for coupling wave energy among the mirrors and out of the cavities. The laser medium for each oscillator is located between one of the first mirrors and one port of one of the pairs of conjugate ports. This arrangement utilizes discrete beam splitters within the resonator in order to coherently add two or more laser channels, operating in the TEM_{00} transverse mode; and obtain a single transverse and longitudinal mode (single frequency) output beam.

Techniques have also been developed for external coherent combining of two lobes of a transverse high order mode distribution emerging from a laser [12-13].

5 SUMMARY OF THE INVENTION

There is a need in the art to obtain high-power laser characterized by improved beam quality, stability, and heat dissipation.

The present invention solves the above problems by providing a novel approach for intra-cavity coherent addition of two or more laser beams that enables
10 stable operation. The present invention takes advantage of synchronizing and coherently adding two or more laser oscillators (with one or more gain media), to produce a higher power output, and utilizes various new intra-cavity couplers and resonator cavity configurations in order to add two or more TEM₀₀ mode beams, two or more single high-order-transverse-mode beams, and two or more transverse
15 multimode beams.

Additionally, the technique of the present invention enables one laser beam with the lowest transverse modal content to impose its low transverse modal content on the other participating laser beam(s), so that all beams can be phase locked, as well as phase locked and added coherently within the laser cavity.

20 The present invention also provides for unique couplers incorporated in a laser cavity for coupling between beams propagating through the laser cavity. Such coupler could contain several optical elements on a single glass substrate, and is thus extremely compact and stable against vibrations and thermal drifts.

Thus, according to one broad aspect of the present invention, there is
25 provided a resonator cavity comprising at least one gain medium and end reflectors which define together longitudinal modes of light in the cavity, the cavity further comprising an intra-cavity beam coupler assembly configured to split light impinging thereon into a predetermined number of spatially separated light channels, and to cause phase locking and at least partial coherent combining of the
30 light channels, which have common longitudinal and transverse modes, in a double pass through the beam coupler assembly, the resonator cavity being configured and

operable to produce at least one output combined light channel of a predetermined intensity profile.

It should be understood that the term "*intensity profile*" used herein is determined by the transverse mode content of light.

5 The beam coupling assembly may be configured to provide coherent combining of the light channels to produce the single output combined channel. Alternatively, the beam coupler assembly may be configured to provide partial coherent combining of the channels, where each channel gives away or receives some coupling power to one or more other channels, and thus produce a
10 multiplicity of spatially separated output light channels, which are phase locked.

Preferably, the desired lowest transverse mode content at the output is produced by passing light through the appropriately designed aperture arrangement into at least one channel. The aperture arrangement may be configured as a single-aperture or multiple-aperture arrangement. The single aperture may be located in an
15 optical path of one of the spatially separated channels or all of them, being upstream of the beams coupler assembly (with respect to a direction of light propagation from the rear end reflector to the output end reflector); or may be located downstream of the beam coupler assembly so as to be in an optical path of the combined channel propagating towards the output end reflector. Considering the
20 multiple-aperture arrangement, it is located upstream of the beam coupler assembly, each aperture being associated with a respective one of the light channels. It should be noted that "upstream aperture arrangement" with respect to the beam coupler assembly may be located either upstream or downstream of the gain medium.

When the light channels are associated with the same gain medium and the
25 beam coupler assembly is configured as an interferometric coupler assembly with uniform transmission regions, no aperture arrangement may be used, thus resulting in the output in the form of a single large intensity profile (distribution) channel with well defined phase.

According to one embodiment of the invention, in which two or more laser
30 beams are phase locked and coherently added, the beam coupler assembly is an interferometric coupler assembly. In the simplest implementation of such an

interferometric coupler, the coupler, formed with discrete and separate elements, is a beam splitter/combiner of predetermined transmission/reflection, for example a beam/splitter combiner disclosed in the above-indicated U.S. Patent 3,414,840. Considering N gain media in the resonator cavity producing N light channels, respectively, the beam coupler assembly includes $(N-1)$ simple beam splitter/combiners.

In another possible implementation of the interferometric coupler, the coupler is a planar interferometric two-beam coupler. The coupler is formed of a high precision plane parallel plate with specially designed coatings. According to yet another possible implementation, the coupler is a planar interferometric N -beam coupler. This coupler is somewhat more complex than the simple two-beam coupler, and is used for intra-cavity phase locking and subsequent coherent addition of more than two laser beams.

The planar interferometric coupler element for coherent addition is preferably a plane parallel plate with its front or rear facet or each of the front and rear facets having a predetermined pattern formed by regions of different transmission/reflectivities. The plane parallel plate has a predetermined thickness d and is oriented with respect to a light propagation axis at a predetermined angle defining a certain angle α of light incidence onto the plate so as to ensure said splitting and said at least partial coherent combining of the light channels in the double pass through the plate.

For the incident angle α , the thickness d of the plate is determined as:

$$d = x_0 / \{ 2 \cos \alpha \operatorname{tg}[\arcsin(\sin \alpha / n)] \}$$

wherein x_0 is a distance between propagation axes of the light channels, and n is a refractive index of a material of the plate, thereby providing for matching the distance between the light channels so as to enable an optimal overlap between the light channels and their collinear propagation after exiting the beam coupler assembly.

The regions of the different reflectivities on the front facet include a substantially transmitting region (e.g., with an anti-reflecting coating), so as to transmit most, if not all, of the incident light, and include at least one region of a

predetermined beam splitting property. The regions of the different reflectivities on the rear facet include a relatively large highly reflective region, and may include a substantially transmitting region (e.g., an anti-reflecting coating).

Generally, the need for anti-reflecting coatings can be eliminated by
5 orienting the beam coupler at a Brewster angle with respect to the cavity axis, and by operating with a specific linear polarization of light.

When operation of the beam coupler assembly in the reflection mode is desired, it is implemented by locating the output end reflector in the optical path of a light portion reflected from the beam splitting region on the front facet of the
10 beam coupler assembly; and optionally also providing the entirely highly reflective rear facet of the beam coupler assembly with the beam splitting region on the front facet being located between two light transmitting regions. In the latter case, care should be taken to appropriately align the end reflector so as to be in an optical path of light propagation from the reflective rear facet through the light transmitting
15 region of the front facet and be outside an optical path of light reflected from the beam splitting region of the front facet.

The dimensions of the regions of different reflectivities of the front and rear facets and the orientation of the plane parallel plate is such that: the substantially transmitting region of the front facet is aligned with the highly reflective region of
20 the rear facet thereby allowing light passage through the plate to the highly reflective region where it is reflected towards the beam splitting region in the front surface and then the light is reflected towards the highly reflective region, and so on; and optionally, especially when operation in the transmission mode is required, one beam splitting region of the front facet is aligned with the substantially
25 transmitting region of the rear facet, so that the light propagation through these regions defines a light output of the beam coupler.

The front facet of the plane parallel plate may comprise the single beam splitting region, thereby producing two light channels. Generally, the front facet has the substantially transmitting region (e.g., anti-reflective coating) and $(N-1)$ beam
30 splitting regions for N light channels, respectively. Each i -th beam splitting region, $i=2, \dots, N$, has a reflectivity of $(1-1/i)$ or a transmittance of $1/i$, such that the first light

channel is substantially not affected by the front facet and the other $(N-1)$ light channels are differently affected by the $(N-1)$ beam splitting regions, respectively.

The planar interferometric coupler assembly may comprise the single plane parallel plate with the patterned front and rear facets. Alternatively, the
5 interferometric coupler assembly may include a pair of first interferometric coupler elements (e.g., the above-described patterned plane parallel plates) associated with a pair of the gain media, respectively, and operating to produce two combined light components, respectively; and a second interferometric coupler element (e.g., the patterned plane parallel plate) for coupling these two combined light components,
10 to produce the single output coherently combined channel.

The interferometric coupler assembly may be configured as a phase locking coupler assembly. Similarly, this is preferably a plane parallel plate with patterned front and rear facets, which has a predetermined thickness and predetermined orientation with respect to the cavity axis. The regions of the different reflectivities
15 on the front facet include a substantially transmitting region (e.g., with an anti-reflecting coating) and at least one region of a predetermined partially light transmitting property, and the regions of the different reflectivities on the rear facet include at least one region of a predetermined partially light transmitting property and a substantially transmitting (anti-reflecting) region. The dimensions of these
20 regions and the orientation of the plane parallel plate are such that one partially transmitting region of the front facet is aligned with the substantially anti-reflecting region of the rear facet. The substantially anti-reflecting region of the front facet is aligned with the partially transmitting region of the rear facet thereby allowing light passage through the plate to the partially transmitting region on the rear facet. Light
25 is reflected from the partially transmitting region of the rear facet towards the partially transmitting region of the front facet; and then light is reflected back towards the partially transmitting region on the rear facet, and so on.

According to another embodiment of the invention, the beam coupler assembly is configured for polarization coupling of the light channels. Polarization
30 couplers are based on exploiting the polarization state of the beams and the effect of conventional polarizers on this state. The polarization coupler assembly includes

two polarizers accommodated in a spaced-apart relationship along the cavity axis; and an optical element configured as a $\lambda/2$ retardation plate or 45° polarization rotator accommodated between the two polarizers.

As indicated above, the aperture arrangement may be configured to define a
5 single aperture or multiple apertures. The aperture has a diameter capable of selecting the desired lowest transverse mode content from the light passing therethrough, which may be Gaussian mode distribution, the desired multiple-transverse-mode distribution, or single high-order transverse-mode distribution in which case an appropriate phase element is used.

10 According to yet another aspect of the invention, there is provided a resonator cavity comprising at least one gain medium and end reflectors which define together longitudinal modes of light in the cavity, the resonator cavity further comprising:

(a) a beam coupler assembly configured to split light impinging thereon into a
15 predetermined number of spatially separated light channels, and to cause phase locking and coherent combining of the light channels, having common longitudinal and transverse modes, in a double pass through the beam coupler assembly, to thereby produce an output combined light channel, the beam coupler assembly being configured for polarization
20 coupling of the light channels and comprising two polarizers accommodated in a spaced-apart relationship along an axis of the cavity; and an optical element configured as a $\lambda/2$ retardation plate or 45° polarization rotator accommodated between the two polarizers; and

(b) an aperture arrangement configured to select in at least one of the light
25 channels a predetermined transverse mode that is desired at the cavity output.

According to another aspect of the present invention, there is provided a beam coupler element for use in a resonator cavity for affecting the light propagation through the resonator cavity to provide an output light channel in the
30 form of coherent addition of at least two light channels having at least one common longitudinal mode, the beam coupler assembly comprising:

- a plane parallel plate with its front and rear facets being patterned to have regions of predetermined transmission or reflectivities, wherein
- the front facet includes a substantially transmitting region and $(N-1)$ beam splitting regions for N light channels, respectively, each i -th beam splitting region, $i=2, \dots, N$, having a reflectivity of $(1-1/i)$ or a transmittance of $1/i$, such that the first light channel is substantially not affected by the front facet and the other $(N-1)$ light channels are differently affected by the $(N-1)$ beam splitting regions, respectively;
- the rear facet includes a highly reflective region; and
- dimensions of said regions of the front and rear facets and orientation of the plane parallel plate with respect to the light channels' propagation axis are such that light is reflected from the highly reflective region towards the beam splitting region and *vice versa*.

According to yet another aspect of the present invention, there is provided a beam coupler element for use in a resonator cavity for affecting the light propagation through the resonator cavity to provide at least two output light channels of desired transverse/longitudinal modes, the beam coupler assembly comprising:

- a plane parallel plate with its front and rear facets being patterned to have regions of predetermined transmission or reflectivities, wherein
- the front facet includes a substantially transmitting region and at least one predetermined beam splitting region;
- the rear facet includes a substantially transmitting region and at least one predetermined beam splitting region; and
- dimensions of said regions and orientation of the plane parallel plate with respect to the light channels' propagation axis are such that light is reflected from the beam splitting region of the rear facet towards the beam splitting region of the front facet and *vice versa*.

According to yet another aspect of the present invention, there is provided a beam coupler element for use in a resonator cavity for controlling light propagating through the resonator cavity to provide at least two output light channels of desired

transverse and longitudinal modes, the beam coupler assembly comprising: a plane parallel plate with its front and rear facets carrying first and second gratings, respectively, the first grating splitting the light into various diffraction orders and allowing their propagation inside the plate towards the second grating.

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BRIEF DESCRIPTION OF THE DRAWINGS

In order to understand the invention and to see how it may be carried out in practice, preferred embodiments will now be described, by way of non-limiting example only, with reference to the accompanying drawings, in which:

10 **Fig. 1A** is a schematic illustration of a resonator cavity configuration according to one embodiment of the invention, configured for intra-cavity coherent addition of two Gaussian beam distributions using a single interferometric coupler;

Figs. 1B and 1C are schematic illustrations of resonator cavities according to another embodiment of the invention, exemplified as being configured for intra-
15 cavity coherent addition of two Gaussian beam distributions using a single interferometric coupler;

Fig. 2 is a schematic illustration of a resonator cavity configuration according to yet another embodiment of the invention, configured for intra-cavity pair coherent addition of four Gaussian beam distributions using interferometric
20 couplers;

Fig. 3 is a schematic illustration of a resonator cavity configuration according to yet another embodiment of the invention, configured for intra-cavity sequential coherent addition of several Gaussian beam distributions using a single
interferometric coupler;

25 **Fig. 4** more specifically illustrates a planar interferometric coupler used in the example of Fig. 3, designed to phase lock and coherently add N light channels when placed in the resonator;

Fig. 5 is a schematic illustration of a resonator cavity configuration according to yet another embodiment of the invention, configured for intra-cavity
30 coherent addition of two Gaussian beam distributions using a polarization coupler;

Fig. 6 is a schematic illustration of a resonator cavity configuration according to yet another embodiment of the invention, configured for intra-cavity coherent addition of four Gaussian beam distributions using polarization couplers;

5 **Fig. 7** is a schematic illustration of a resonator cavity configuration according to yet another embodiment of the invention, configured for intra-cavity coherent addition of two single high-order TEM_{01} transverse mode beam distributions using a single interferometric coupler;

10 **Fig. 8** is a schematic illustration of a resonator cavity configuration according to yet another embodiment of the invention, configured for intra-cavity coherent addition of two multimode transverse beam distributions using a single interferometric coupler;

Figs. 9A and 9B schematically illustrate the principles of intra-cavity coherent addition of several single (or multiple) mode beam distributions derived from separate fiber lasers using discrete beam splitters couplers, wherein **Fig. 9A** shows intra-cavity sequential addition configuration and **Fig. 9B** shows intra-cavity coherent addition of pairs configuration;

20 **Fig. 10** schematically illustrates yet another embodiment of the invention, where one channel imposes a Gaussian mode on the other channel and coherent addition of the two beams distributions is achieved using a single interferometric coupler;

Fig. 11 schematically illustrates the embodiment of the invention, where one channel imposes a single high-order transverse mode on the other channel and coherent addition of the two high order mode distributions is achieved using a single interferometric coupler;

25 **Fig. 12** schematically illustrates the embodiment of the invention, where one channel imposes a specific multimode content on the other channels and sequential coherent addition of the four beams is achieved using a single interferometric coupler;

30 **Fig. 13** schematically illustrates the embodiment of the invention, where the common channel imposes Gaussian mode content on the two channels and coherent addition of the two beams is achieved using a single interferometric coupler;

Figs. 14 to 16 illustrate yet another embodiment of the invention providing phase locking of laser beams, wherein **Fig. 14** shows intra-cavity phase locking of two Gaussian beam distributions using a single interferometric coupler, **Fig. 15** shows the calculation results for the feedback after a double pass through the coupler of **Fig. 14** for three cases, corresponding to, respectively, incoherent summation of laser beams, and positive and negative coherent summation of the beams; **Fig. 16A** shows intra-cavity phase locking of four Gaussian beam distributions using a single interferometric weak coupler; **Figs. 16B and 16C** show intra-cavity phase locking using a grating-based coupler.

Figs. 17A and 17B schematically illustrate the principles of the present invention aimed at improving the beam quality of multimode resonators, wherein **Fig. 17A** shows the general configuration of the multimode laser resonator and **Fig. 17B** shows a laser resonator of the present invention with an array of 2x2 Gaussian beam distributions; and

Fig. 18 schematically illustrates a possible pulsed Nd:YAG laser experimental setup used for intra-cavity coherent addition of two Gaussian beam distributions.

DETAILED DESCRIPTION OF THE INVENTION

The present invention provides for a novel method for light propagation in resonator cavity and novel resonator cavity configuration enabling intra-cavity phase locking, or intra-cavity phase locking and coherent addition, of two or more laser beams. Various examples of the laser cavity configurations of the present invention are described below. The configurations, as well as light propagation schemes, are shown in the figures schematically, and it should be understood that these configurations could be realized with basically all types of stable resonators (various mirror curvatures or other intracavity optical elements), with various types of gain mediums (gas, solid-state, diode, fiber, etc.), with various types of operational methods (CW, pulsed free running, Q-switched pulsed, etc.); etc.

Referring to **Fig. 1A**, there is schematically illustrated an example of a resonator cavity, generally at **10A**, configured for intra-cavity phase locking and

coherent addition of two light channels. The resonator cavity **10A** typically includes a back mirror arrangement **12** and an output coupler **14** (constituting end reflectors, respectively), and a gain medium **16** (laser rod), which together define the longitudinal modes (frequencies) of the cavity **10A**. The back mirror **12** is preferably flat, while the output coupler **14** may be either flat or concave for stable laser operation. According to the invention, the resonator cavity **10A** further includes a beam coupler assembly **20** accommodated downstream of the gain medium **16** (with respect to a direction of light propagation from the back mirror arrangement **12** to output coupler **14**), and in the present example also includes an aperture arrangement **18**, which in the present example is accommodated between mirror **12** and gain medium **16**. Generally, the aperture arrangement, when accommodated upstream of the beam coupler assembly, may be positioned either upstream or downstream of the gain medium. As will be exemplified further below, the aperture arrangement may be associated with a combined output channel propagating towards the output end reflector **14**.

Generally, the beam coupler assembly of the present invention is configured to split the laser light into a predetermined number of spatially separated light channels and to cause either a partial combining of the light channels, or coherent addition of the light channels with common longitudinal modes (frequencies) and common transverse modes, to thereby produce one or more output combined light channel(s). The beam coupler assembly is configured to involve a loss mechanism whereby the beams do not suffer any loss in case of a specific relative phase between the beams, and suffer severe losses otherwise.

The aperture arrangement is configured to select in at least one light channel a predetermined transverse mode content (determining the intensity profile) that is desired at the cavity output.

In the present example of **Fig. 1A**, the cavity **10A** is configured for coherently adding two Gaussian TEM_{00} beam distributions. Consequently the aperture arrangement **18** includes a double-aperture with diameters suitable for fundamental TEM_{00} operation in each of the two channels. The beam coupler

assembly **20** is configured for interferometric coupling and includes a single coupling element in the form of a planar interferometric two-beam coupler.

It should be noted that instead of using the single gain medium (laser rod) with two channels, two separate laser rods can be used. In this case, a back mirror arrangement (**12** in Fig. 1) could include two back mirrors associated with two laser rods, respectively.

The beam coupler **20** is configured as a high precision plane parallel plate **21**, with the front and rear facets of the plate having specially designed patterns, namely, regions of different transmission/reflectivity. The front facet has a substantially light transmitting region **21A** (e.g., coated with an anti-reflection layer) and a beam splitting region **21A'**, and the rear facet has a substantially light transmitting region **21B** (e.g., coated with an anti-reflection layer) and a highly reflective region **21B'**.

It should be noted that in this example, as well as in all other examples, by orienting the beam coupler at a Brewster angle with respect to the cavity axis **OA** and operating with a specific linear polarization of light the need for anti-reflecting coatings is eliminated.

The plate **21** has a predetermined thickness d and is oriented with respect to the cavity axis **OA** (i.e., to the laser beams) at a predetermined angle defining a certain angle α of light incidence onto the plate **21** selected in accordance with the required distance between two beams **A** and **B** thus providing for the two beams optimal overlapping and collinear propagation after exiting the coupler through the anti-reflective region **21B** (i.e., to ensure the splitting and coherent addition of two light channels). For an incident angle α , thickness d of the plate **21** is determined by the simple relation:

$$d = x_0 / \{ 2 \cos \alpha \operatorname{tg}[\arcsin(\sin \alpha / n)] \}$$

where x_0 is the distance between the two beams **A** and **B**, and n is the refractive index of the material of the plate **21**.

The dimensions of the pattern regions and the orientation of the plate **21** are such that the light transmitting region **21B** and the beam splitting region **21A'** are aligned, so as to define the output of the coupler **20** for the combined channel **C**,

and the light transmitting region **21A** and the highly reflective region **21B'** are aligned so as to ensure that light is reflected from the highly reflective region **21B'** towards the beam splitting region **21A'**. Thus, the beam of one channel **A** is directly incident on the beam splitting region **21A'**, while the beam of the other channel **B** is transmitted through the region **21A**, reflected back from the rear facet region **21B'** and is incident on the beam splitter coating **21A** so as to be collinear with the transmitted beam **A**.

In this specific example, where the channels are produced by the same gain medium **16**, input beams **A** and **B** are of substantially equal intensities. Accordingly, one half **21A** of the front facet is substantially transmitting and the other half of this facet is coated with a 50% beam splitter layer **21A'**, while half of the rear facet is coated with the highly reflecting layer **21B'** and the other half **21B** of this facet is substantially transmitting. It should be understood that in case of different intensities of the input beams **A** and **B** (different gain levels), an appropriate transmission of the beam splitting region **21A'** of the coupler **20** should be chosen.

If the input beams **A** and **B** incident on the 50% beam splitter are in phase, there would be no loss. If the two input beams have a π -phase difference, then destructive interference would occur and there would be 100% losses. If the input beams have random relative phase between them (incoherent), then each beam will suffer 50% loss at the coupler **20**, so, typically, no lasing will occur. Hence, if the beams add coherently, then the losses introduced by the coupler **20** may be completely suppressed. Indeed, the combined laser will tend to operate so that the losses are minimum, whereby the phases of the individual beams will be automatically matched (automatic phase locking) such that coherent addition takes place. This of course can be achieved only for those longitudinal modes (frequencies) that are common in the two laser channels. Thus, care must be taken to either perfectly equalize the optical length of the two resonator channels, or alternatively, to imbalance them in such a manner so as to obtain one or more mutual longitudinal modes. To this end, additional optical elements, such as optical cubes or plates, could be inserted into the channels to obtain the appropriate optical path lengths.

It should be noted that an appropriate design of the optical path length difference between the intracavity channels, taking into account the gain bandwidth, could result in a single frequency output (or very narrow linewidth output) from the resonator cavity. In the resonator cavity configuration utilizing a single-coupler
5 assembly (for example as that exemplified in Fig. 1A), slight tilting of the interferometric plate results in wavelength tuning within the gain bandwidth. This could be implemented using for example a piezo motor, achieving very fast tuning rates.

The above-described example of **Fig. 1A** presents the transmission mode
10 configuration of a resonator cavity. Referring to **Figs. 1B and 1C**, there are shown two examples, respectively, of a resonator cavity configured for the reflection mode operation. To facilitate understanding, the same reference numbers are used for identifying those components that are common in all the examples of the invention. Resonator cavities **10B** and **10C** are shown, each configured generally similar to
15 the above-described resonator cavity **10A**, namely, including end reflectors **12** and **14**, a gain medium **16**, an interferometric beam coupler assembly **20** configured as a high precision plane parallel plate **21**, and an aperture arrangement **18**. In these examples, in distinction to that of Fig. 1A, the output coupler **14** is located in an optical path of a light portion reflected from the beam coupler assembly **20** and
20 emerging from the front facet thereof. In the example of **Fig. 1B**, the interferometric plate **21** is similar to that of Fig. 1A, namely, includes light transmitting and beam splitting regions **21A** and **21A'** on the front facet, and highly reflective and transmitting regions **21B'** and **21B** on the rear facet. In the example of Fig. 1C, the interferometric plate **21** has a somewhat different pattern of reflective/transmitting
25 regions on its front and rear facets: the rear facet is entirely highly reflective **21B'** and the front facet has a beam splitting region **21A'** surrounded by substantially light transmitting regions **21A**. In this case, however, the output coupler (mirror) **14** is configured and positioned so as to be in an optical path of a light portion reflected from the rear facet and passing through the transmitting region of the front facet and
30 to be outside an optical path of a light portion reflected from the beam splitting region of the front facet.

The configurations of Figs. 1A-1C can be generalized to intra-cavity coherent addition of more than two beams. This is exemplified in Fig. 2 for the transmission mode configuration. Fig. 2 shows a resonator cavity 100 configured to provide for automatic phase locking and coherent addition of four Gaussian beam distributions B_1 - B_4 to form a single Gaussian TEM_{00} output beam C. This addition method will be referred to as "*pair addition*", since the beams are added in pairs. It should be understood that the pair addition could be extended to more than two beam pairs. In this technique, all laser channels have at least one mutual longitudinal mode (frequency), which might be easier to achieve with a smaller number of laser channels.

The device 100 includes a pair of back mirrors 12A and 12B; gain media 16A and 16B (laser rods) associated with the mirrors 12A and 12B, respectively; a pair of double-aperture arrangements 18A and 18B associated with laser rods 16A and 16B, respectively; an interferometric beam coupler assembly 120; and an output coupler 14. The diameter of each of the apertures is such as to select a Gaussian beam distribution from the respective channel. The beam coupler assembly 120 includes two interferometric couplers 20A and 20B accommodated in optical paths of light passing through the laser rods 16A and 16B, respectively; and an additional planar two-beam interferometric coupler 20C downstream of the couplers 20A and 20B (with respect to the direction of light propagation from the back mirror 12 to the output coupler 14).

The front and rear facets of each of the couplers 20A and 20B are partially coated with, respectively, a 50% transmitting coating 21A' and a highly reflective coating 21B'. The couplers 20A and 20B are configured and oriented such that their coating-patterns (50% transmitting and highly reflective regions 21A' and 21B) are positioned symmetrically identical with respect to the cavity axis OA. The coupler 20C is a planar interferometric two-beam coupler as that described above with reference to Fig. 1A.

Coupler 20A (when in the resonator cavity) operates to perform phase locking and coherent addition of channels B_1 and B_2 , produced by gain medium 16A, resulting in a combined beam C_1 . Coupler 20B performs phase locking and

coherent addition of channels B_3 and B_4 , produced by gain medium $16B$, resulting in a combined beam C_2 . Coupler $20C$ carries out coherent addition of beams C_1 and C_2 , resulting in a combined output channel C .

Fig. 3 schematically illustrates another example of a resonator cavity configuration **200** for intra-cavity sequential coherent addition of more than two Gaussian beams. The resonator cavity device **200** includes a back mirror **12**; a gain medium **16**; a multi-aperture arrangement **218**; a beam coupler **220** including a single planar interferometric n -beam coupler; and an output coupler **14**. The aperture diameters are adjusted to select the Gaussian mode.

The beam coupler **220** is somewhat more complex than the above-described two-beam coupler, and is used for intra-cavity phase locking and sequential coherent addition of more than two laser beams. The coupler **220** is made of a high precision plane parallel plate **21**, with most of its back (rear) facet being coated with a highly reflective layer **21B'** and the rest being a substantially transmitting region **21B**, while the front facet has 4 sub-areas for 4 light channels, respectively: the first sub-area **21A** (associated with the first channel B_1) is substantially transmitting (zero reflectivity) and the other three sub-areas $21A^{(2)}$ - $21A^{(4)}$ (associated with channels B_2 - B_4 , respectively) are coated with different beam-splitter coatings having different transmittance, respectively, namely, 50%, 33.3% and 25%. Minimal loss is obtained in this configuration if channel B_1 is coherently added (at the 50% coating) with channel B_2 , the so-produced combined channel C_1 coherently add with channel B_3 (at the 33% coating), and the combined channel C_2 coherently add with channel B_4 (at the 25% coating) to produce a combined output channel C_3 .

Under certain conditions, the laser **200** (resonator cavity) will tend to operate such that all channels phase lock and add up coherently, so that a Gaussian TEM_{00} beam with increased power is obtained at the output. To ensure that there is at least one common longitudinal mode (frequency), additional optical elements, such as optical cubes or plates, could be inserted into the channels to obtain the appropriate optical path lengths.

In the present example of **Fig. 3**, the coupler **220** is designed to phase lock and coherently add four beams. It should, however, be understood that a similar beam coupler assembly can be used to coherently add a larger number of beams. A more general coupler configuration is illustrated in **Fig. 4**, showing an intra-cavity beam coupler **1220** configured for phase locking and coherent addition of n beams with common longitudinal modes (frequencies) and common transverse mode (e.g., Gaussian mode). The coupler **1220** is made of a high precision plane parallel plate **21**, with most of its back (rear) facet being coated with a highly reflective layer **21B'** and the rest being a substantially transmitting region **21B**, and the front facet having N sub-areas for N light channels, respectively: first sub-area (associated with the first channel) being substantially transmitting **21A** (zero reflectivity) and the other $(N-1)$ sub-areas being coated with different beam-splitter coatings, generally at **21A⁽ⁱ⁾** ($i=2,\dots,N$) having different reflectivities, respectively. Generally, each i -th beam splitting region has a reflectivity of $(1-1/i)$ or a transmittance of $1/i$, such that the first channel is substantially not affected by the front facet and all the other channels are differently affected by the $(N-1)$ regions with transmittance 0.5, 0.33, ..., $1/N$, respectively.

For each orientation and/or thickness of the beam coupler **1220**, there exists a specific relative phase between two consecutive beams which causes all the beams **B₁-B_n** to coherently add at the output of the beam coupler **1220**, producing an increase in output power by a factor of n . If the relative phase between the input beams has a different value or is random, then the beams would suffer losses. In this coupler, the first beam **B₁** is added with the second beam **B₂**, then the so-produced combined beam is added with the third beam **B₃**, and so on. Hence, each beam is sequentially added to the previously combined beams.

It is important to note and is clearly understood for example from the illustration in **Fig. 4**, that each of the interferometric coupler configurations of the present invention introduces a constant optical path difference ΔL between the optical paths of each two successive channels **B_i** and **B_(i+1)**, considering N light beams ($i=1,\dots,N$). It should be understood that the optical path length L_i of the channel of beam **B_i** is the optical distance between the rear and output end reflectors

12 and 14 and the point where the combined channel starts. Thus, the optical path lengths of the channels $B_1 - B_N$ are L_I , $L_I + \Delta L$, $L_I + 2\Delta L$, and so on, and the optical length difference between these channels is an integer number of ΔL , namely $n\Delta L$. This configuration ensures common longitudinal modes (frequencies) in all the
5 beams.

It should be noted that in all the configurations described above, if the gain in each channel is different, such that the power of the different channels is unequal, then appropriate beam splitter transmissions should be used.

Reference is now made to **Fig. 5** illustrating a resonator cavity configuration
10 **300** according to another embodiment of the invention. The cavity **300** is configured for intra-cavity coherent addition of two Gaussian beam distributions using polarization coupling. The device **300** includes back mirrors **12A** and **12B**, gain media **16A** and **16B**, single-aperture arrangements **318A** and **318B**, a beam coupler assembly in the form of polarization coupler arrangement **320**; and an
15 output coupler **14**. The configuration defines light propagation channels C_1 and C_2 .

Polarization couplers are based on exploiting the polarization state of beams and the effect of conventional polarizers on this state. The coupler assembly **320** includes two polarizers **322A** and **322B** and an optical element **323** configured as a $\lambda/2$ retardation plate or 45° polarization rotator.

20 Minimal losses at polarizer **322A** occur if channel C_1 has pure p -polarization and channel C_2 has pure s -polarization. If the $\lambda/2$ retardation plate **323** (or 45° polarization rotator) is aligned so as to change the polarization plane by 45° , then minimal losses at polarizer **322B** are achieved only if the two beams C_1 and C_2 have a specific relative phase when reaching polarizer **322B** (0 or π phase,
25 depending on whether the polarization was changed by $\pm 45^\circ$). If, for example, the beams C_1 and C_2 have the correct polarization states but the relative phase between the beams is random, then each beam suffers 50% loss when passing through the coupler. Hence, this coupler **320** coherently adds only two beams with specific polarizations and relative phase at the input. It is thus evident that with the
30 polarization coupler **320**, minimal losses are obtained if channel C_1 is p -polarized

and channel C_2 is *s*-polarized, and if both are in phase. In this case, the laser **300** will tend to arrange the polarization state and the phases such that minimal loss state is obtained.

It should be noted that instead of using the $\lambda/2$ retardation plate or the 45° polarization rotator, it is possible to align the second polarizer **322B** at a 45° , and achieve the same performance. It is also possible to reduce/control the losses to the undesired phase states by using a series of Brewster plates instead of the polarizer **322B**.

The above concept can be generalized to pair addition of more than two Gaussians. This is exemplified in **Fig. 6** showing a resonator cavity **400** configured for intra-cavity coherent addition of four Gaussian beams. The cavity **400** is formed by two arrangements **402** and **404** each including all the elements of the above-described device **300** except for output coupler (namely, includes back mirrors, apertures, gain media, and polarization coupler); an additional common polarization coupler **420'**; a $\lambda/2$ or 90° rotator **423'** in the optical path of light output from one of the arrangements **402** and **404** - arrangement **404** in the present example; and an output coupler **14**. The polarization coupler **420'** is configured generally similar to coupler **320**, namely includes two polarizers **422A** and **422B** and a $\lambda/2$ retardation plate or 45° polarization rotator **423** therebetween.

The present invention also provides for obtaining increased output power from a resonator cavity, by intra-cavity phase locking and coherent addition of single high-order mode beams. This can be implemented by introducing an appropriately designed phase element (or any other suitable mechanism, such as absorptive wires, phase strips, etc.) into the resonator cavity of each of the above-described configurations to select the same single high-order mode in each of the channels. The principles of using phase elements in order to select high-order transverse modes are known [14].

Fig. 7 shows a laser cavity **500** configured for intra-cavity coherent addition of two single high-order TEM_{01} transverse mode beam distributions using a single interferometric coupler. The device **500** includes a back mirror **12**; a double aperture arrangement **518**; a phase element **505**; a gain medium **16**; a beam coupler

assembly **20**; and an output coupler **14**. Here, the aperture's diameter is adjusted to select a high-order mode distribution. The beam coupler **20** is a planar two-beam interferometric coupler as described above. As shown in the figure, the phase element **505** creates a π -phase step for each of two channels C_1 and C_2 and thus
5 selects the TEM₀₁ mode distribution in each channel. If light components from the two channels are added incoherently, each light component will suffer 50% losses. With coherent addition, the laser will "chose" to operate such that the two high-order mode beams are phase locked and coherently add at the beam coupler **20**. The use of this concept of intra-cavity phase locking and coherent addition of single
10 high-order mode beams provides for obtaining higher output powers than with Gaussian beam combining, and provides for the potential beam quality of the high-order mode beam at the output to be as good as that of a Gaussian distribution.

The technique of the present invention also provides for intra-cavity coherent addition of transverse multimode beams. This is exemplified in **Fig. 8**,
15 showing a resonator cavity configuration **600**, which is generally similar to that of Fig. 1 for coherent addition of two Gaussian beams, but distinguishes therefrom in that the double apertures arrangement **618** has diameters that enable transverse multimode operation in both channels. Minimal loss to both beams at the beam coupler **20** will be achieved if each of the transverse mode distributions in the first
20 channel is phase locked and coherently adds with the corresponding mode distribution in the second channel. Specifically, each individual mode distribution of the overall multimode distribution in one channel will be phase locked and coherently add up to those of the multimode distribution in the other channel: the TEM₀₀ mode in both channels will be phase locked and will coherently add up, the
25 TEM₀₁ mode in both channels will be phase locked and will coherently add up, and so on. In this case, the resonator cavity **600** will "chose" to operate in this minimal loss state, so that the output beam is a multimode beam (with the same beam quality factor, M^2 , as that of the single channel beam) but with twice the power. This can be looked upon as coherent addition of multimode beams, where each transverse mode
30 is coherently added, but there is random phase between the various transverse modes.

It should be noted that, generally, each of the above-described examples of the resonator cavity of the present invention can be used to intra-cavity phase lock and coherently add two or more transverse multimode beams, provided suitable apertures are used. Moreover, channels with the same multimode distribution content but different powers can be added coherently, using suitable couplers (with appropriate beam splitting region(s)).

The inventors have found that the resonator cavity may utilize a simple beam splitter coupler for intra-cavity coherent addition of multimode beams (using suitable apertures) or for intra-cavity coherent addition of single high-order mode beams (using, in addition, suitable phase elements as described above). **Figs. 9A and 9B** illustrate the principles of intra-cavity coherent addition of several beam distributions derived from separate fiber lasers using discrete beam splitters couplers.

Fig. 9A exemplifies intra-cavity sequential addition configuration. A resonator cavity **700A** is shown including back mirrors **12A-12E**; gain media **16A-16E** (e.g., double-clad fibers); a beam coupler assembly including simple beam splitter couplers **120A-120D**; and an output coupler **14**. The couplers **120A-120E** have 50%, 33.3%, 25% and 20% reflectivities, respectively. Collimation lenses **L₁-L₅** are provided in each of the channels, respectively.

Thus, each of the couplers **120A-120D** is a beam splitter of predetermined transmission/reflection. As specifically shown for example for beam splitter **120A**, beams **B₁** and **B₂** (coming from gain media **16A** and **16B**, respectively) impinge onto the beam splitter **120A**, resulting in an output beam **C₁** (and possibly also a losses energy part). If input beams **B₁** and **B₂** have equal intensities and undergo the 50% beam splitting by the coupler **120A**, then (1) for the two beams being in phase they coherently add at the beam splitter **120A** and no losses occur, (2) at a π phase difference between the beams they interfere destructively at the beam splitter and there are 100% losses, and (3) at random relative phase between input beams **B₁** and **B₂** (incoherent) each beam suffers 50% loss at the beam splitter **120**. If the input beams **B₁** and **B₂** do not have equal intensities, a suitable transmission should

be chosen for the beam splitting region of the coupler **120A** in order to achieve perfect coherent addition when the beams are in phase.

Thus, the device **700A** provides for sequential coherent addition of beams **B₁-B₅** during their propagation towards the output coupler **14**: beams **B₁** and **B₂** are coherently added at the coupler **120A** and a resulting combined beam (**C₁**) is added to beam **B₃** at coupler **120B**, and so on.

Fig. 9B exemplifies intra-cavity coherent addition of pairs in a resonator cavity **700B** including back mirrors **12A-12D**; gain media **16A-16D**; a beam coupler assembly including simple interferometric couplers **120A-120C**; and an output coupler **14**. Coupler **120A** coherently adds channels **C₁** and **C₂**, coupler **120B** adds channels **C₃** and **C₄**, and the resulting combined channels are added at coupler **120C**.

It should be noted, although not specifically shown, that the beam splitters **120A-120C** may be replaced by appropriately designed fiber couplers, for example fiber couplers suitable for coupling light from single-mode fibers [9-11], or those capable of coupling light from multi-mode fibers.

Furthermore, the technique of the present invention provides for imposing the transverse modal content of one beam (one laser channel) on one or more of laser channel beams, and then coherently adding all the beams. This can be achieved with any one of the above-described cavity configurations and coupler designs, provided a suitable aperture is used. It should be noted that although in the above-described examples, an aperture was provided in each of the channels, it is possible to use only one suitable aperture in one channel and this will automatically impose the same mode distribution on the other channels. The following are some examples of laser cavity configurations utilizing this concept.

Fig. 10 shows a resonator cavity **800** including a back mirror **12**; an output coupler **14**; a gain medium **16**; a single-aperture arrangement **818** in one channel associated with laser beam **B₁**; and a beam coupler assembly including a planar two-beam interferometric coupler **20**. In the present example, the aperture **818** is configured to select a Gaussian mode from one channel only (that of beam **B₁**), and at the coupler **20** a Gaussian mode of this channel is imposed on the other channel

(beam B_2), and coherent addition of the two beams' distributions is thus achieved. The operation of this resonator cavity can be understood by considering the losses to various transverse modes in the aperture-less channel (beam B_2). All of the transverse modes, except for the mode present in the other channel B_1 , will suffer considerable losses at the intra-cavity coupler **20**, and, if the gain is not too high, these modes will not lase. On the other hand, the common mode for the two channels will suffer no losses and will coherently add. Thus, both the imposing of the modal distribution content and the coherent addition are achieved.

Fig. 11 illustrates the case when a single high-order mode is desired at the output, and thus a single aperture and a single phase element are required in only one of the channels. A resonator cavity **900** is shown differing from that of Fig. 10 in that the single-aperture arrangement **918** and a phase element **905**, configured to create a π -phase step, are located in one channel/beam B_2 . Hence, one channel imposes a single high-order transverse mode on the other channel, and coherent addition of the two high order mode distributions is achieved using the single interferometric coupler **20**. It should be noted that the aperture and/or the phase element may be positioned in either one of the channels (including the output combined channel).

Fig. 12 exemplifies the case when obtaining a specific multimode beam (say with $M^2=3$) at the output is desired. A resonator cavity **1000** includes a back mirror **12**; an output coupler **14**; a gain medium **16**; and a planar interferometric beam coupler **220** (configured as described above with reference to Figs. 3 and 4); and a single-aperture arrangement **1018** in optical path of one of four laser beams B_1 - B_4 - beam B_1 in the present example. The beam coupler **220** is appropriately patterned with coatings: a highly reflective coating on its rear facet, and 50%, 33.3, and 25% beam splitting coatings on its front facet. Here, the single suitable aperture **1018** is provided in one of the channels, and thus one channel imposes a specific multimode content on the other channels, and the use of the single interferometric coupler **220** provides sequential coherent addition of the four beams.

It should be noted that a resonator cavity of the present invention may utilize two interferometric plates with multiple coatings, similar to those of Figs. 3, 4 and

12, to generate two-dimensional arrays of beams. This can be implemented by orienting one plate at a certain vertical tilt angle with respect to a plane perpendicular to the cavity axis thus accounting for coherent addition in the vertical direction, while orienting the second plate at a certain horizontal tilt angle with respect to said perpendicular plane and accounting for coherent addition in the horizontal direction. This results in coherent addition of large arrays (3x3, 4x4, 5x5, 6x6, etc.) with the use of only two multiple-coating interferometric plates. An example of such configuration will be described further below with reference to Fig. 17B.

10 **Fig. 13** shows a resonator cavity **2000** including a back mirror **12**, an output coupler **14**, a gain medium **16**, a beam coupler assembly including a planar two-beam interferometric coupler **20**; and a single-aperture **2018** located in the common (combined) channel **C**. Using only a single aperture in the common channel, where the two or more channels coincide, introduces losses to the common multimode beam at the output of the coupler **20**, so that only the desired Gaussian or multimode beam (depending on the aperture diameter) will lase. If a single high-order mode operation is desired, then also a single phase element or other mode selecting element in one of the channels or in the combined channel is needed, in which case only a specific single high-order mode beam will lase.

20 It should be noted that all the above-described configurations provide for achieving intra-cavity phase locking of laser beams, because in order to coherently add beams they must be phase locked. With all the above configurations it is possible to use a highly reflective mirror as the output coupler **14** and change the back mirrors **12** by output couplers, and thus obtain several phase locked beams at the output. The above-described configurations involve strong coupling between the channels, which might be undesired with low gain lasers.

25 The present invention provides for intra-cavity phase locking of laser beams with "weak" couplers. Referring to **Fig. 14**, there is illustrated a resonator cavity **3000** configured for intra-cavity phase locking of two laser beams with a phase locking beam coupler assembly. The device **3000** includes a back mirror **12**, an output coupler **14**, a gain medium **16**, a double-aperture arrangement **18**, and a

phase locking interferometric coupler **420**. This coupler **420** is related to the above-described couplers, but is used here to perform only the phase locking and not the coherent addition of the beams into a single output beam. The coupler **420** is generally similar to the coupler of Fig. 1 (planar interferometric two-beam coupler), but distinguishes therefrom in that a high reflection coating (**21B'** in Fig. 1) and a 50% beam splitter coating (**21A'** in Fig. 1) are both replaced by partially transmitting coatings **25**. The coating **25** may, for example, be of 80% transmission. In case of different intensities of input beams **A** and **B**, different appropriate transmission values should be chosen for the two coatings. If the two input beams **A** and **B** are not phase coupled (random relative phase), then each beam will suffer about 30% loss at the coupler **420** in a double pass, namely, traveling once through the coupler **420** and then back again through the coupler **420**. But if the input beams **A** and **B** are phase coupled, such that the two beams add up coherently on the coupler **420** (forward and back), then the losses for both beams at the coupler are negligible.

Thus, in the configuration of **Fig. 14**, the two beams are transmitted through the coupler **420**. If they are in phase, then in one direction the first channel will pass off power to the second channel (coherent addition at the second beam splitter), while in the reverse direction the second channel will pass off power back to the first channel (coherent addition on the first beam splitter). So, the coupler is sort of a directional tap, enabling exchange of power between the channels.

Considering the interferometric coupler **420** and the output coupler **14** with $R=1$ as one feedback mechanism into the laser, then the feedback versus the transmission of the beam splitters on the interferometric coupler is as illustrated in **Fig. 15**. These are calculation results for the feedback after a double pass through the coupler **420**, assuming a 100% reflectivity mirror placed at the output of the coupler. Three graphs G_1 - G_3 are shown, corresponding to, respectively, incoherent summation of the beams, and positive and negative coherent summation of the beams. It is thus evident that, with the correctly chosen conditions, even a small coupling percentage (i.e., low reflection percentage) is sufficient to produce big discrimination between the positive coherent summation and the incoherent

summation. It should be noted that choosing slightly different transmissions for the beam splitters could further reduce the losses for the positive coherent summation case.

It can be seen that when the beams are in phase, even with strong couplers (transmission<80%) the feedback is high and the losses at the coupler are insignificant. On the other hand, if the beams are not phase locked and have a random relative phase, then the feedback is much lower, and the losses at the coupler are severe (even with $T=95\%$). In this configuration and with more than a few percentage of coupling the laser will "chose" to operate so that the beams will be phase locked. This will occur only if there is at least one common frequency (longitudinal mode) to both laser channels (it might be necessary to insert additional passive/active optical elements, such as delay plates that can be actively tilted, into the channels to introduce appropriate phase/path delays).

Fig. 16A schematically illustrates how weak coupling can be created between more than two channels by using a sequential coupler generally similar to that of Fig. 14, but with different coatings. A resonator cavity **4000A** is shown including a back mirror **12**, an output coupler **14**, a gain medium **16**, a multi-aperture arrangement **318**, and a sequential interferometric coupler **520**. The coupler **520** is a plane parallel plate **21** with different partially transmitting coatings on its front and rear facets. More specifically, the front facet has a substantially transmitting region **21A** and $(N-1)$ different partially transmitting (beam splitting) regions, generally at $25A^{(i)}$, three such regions being shown in the present example of, respectively T_1 , T_2 and T_3 transmissions (considering four light channels, i.e. $N=4$). The rear facet has a substantially transmitting region **21B'**, and a region formed by $(N-1)$ different beam splitting sub-regions ($N=4$ in the present example) of, respectively T_4 , T_5 and T_6 transmissions. All the beams **B₁-B₄** are transmitted through the coupler **520**, each giving away or receiving some coupling power to the other channels. The necessary transmissions, so as to maximize the feedback (homogeneously among the channels) and minimize the losses at the coupler, can be calculated for the case when all beams are in phase and coherently add at the coupler **520**. Here, at least one mutual longitudinal mode for all possible channels

should exist so that coherent addition can take place (additional passive/active optical elements, such as delay plates that can be actively tilted, that introduce appropriate phase/path delays could be used). Under these conditions, the laser will automatically operate such that all beams are phase locked. It should be noted that it is possible to interchange the back mirror and the output coupler so that the output phase locked beams are to the left.

As also shown in the figure, the above-described resonator cavity **4000A** optionally includes a lens arrangement **LA**. This may be an array of small lenses (lenslets) arranged such that each channel is associated with its corresponding lens. Such an effect of adding curvature to the basic single channel resonator enables better transverse mode selection and less sensitivity to thermal lensing in the gain medium. It should be noted, although not specifically shown, that alternatively or additionally, the output coupler (mirror) **14** may be configured as an array of concave output couplers.

Generally, in order to reduce the effect of thermal lensing on the combining efficiency, when partially or fully coherently adding channels in the same gain medium, the beam coupler assembly could be positioned near the waist of the beam in the cavity (the waist can be designed to be within the cavity by adding intra-cavity mirrors of changing curvature). Alternatively or additionally, an intra-cavity lens (negative) could be used near the gain medium (as exemplified in the configuration of Fig. 16A, being shown dashed curves) in order to reduce the positive thermal lensing effect of the gain medium.

It should also be noted that, for practical implementation, the transmissions at the front and back surfaces of the interferometric coupler **520** could be chosen to be uniform (for example 80% transmission), which provides for a very simple device fabrication procedure, although resulting in some energy loss.

Additionally, it should be noted that when operating with a single large gain medium and an interferometric plate with uniform coatings (as exemplified in Fig. 16A), the phase locking can also be achieved without any aperture. In this case, definite channels are not formed within the resonator, but instead a single large "supermode" distribution with a defined phase is formed at the output. When the

thickness of the interferometric plate is designed adequately, this supermode has a uniform phase and could roughly resemble a very large Gaussian. This could be useful for obtaining an output beam with high power and good beam quality.

It should also be noted that intra-cavity phase locking can be obtained by
5 using a coupler based on specially designed gratings. This is illustrated in **Figs. 16B and 16C**.

Fig. 16B exemplifies a resonator cavity **4000B** configured for phase locking three discrete channels using three spaced-apart apertures. The device **4000B** thus includes a back mirror **12**, an output coupler **14**, a gain medium **16**, a grating-based
10 coupler **620**, and an aperture arrangement **418** defining three apertures. Here, the apertures serve for forming the spatially separated channels. Also, the aperture' diameter defines the transverse mode content in each channel. The coupler **620** is configured as a plane parallel plate with its front and rear facets having patterned regions (surface relief) presenting two specially designed gratings **621A** and **621B**.

15 Light incident on the first grating **621A** is split into light portions of various diffraction orders, and these light portions propagate inside the plate towards the second grating **621B**. The spacing between the adjacent apertures, the thickness of the coupler plate, and the pattern features' dimensions of the gratings, are designed such that light from neighboring channels constructively and destructively interfere
20 at the second grating, thus coupling these channels. In the figure, dotted lines coming out of the coupler **620** indicate light paths where the destructive interference occurs between different diffraction orders of the neighboring channels. Constructive interference between neighboring channels occurs only along the original channel paths designated by solid lines.

25 The gratings should preferably be designed such that most of the energy is distributed between the 0, +1, -1 orders, with low energy in higher diffraction orders. The exact distribution of energy between the 0 order and the +1,-1 orders determines the coupling strength of the coupler.

In order to minimize losses, the resonator cavity self-phase-locks such that
30 constructive interference occurs at the second grating in the original channels and

all other diffraction orders destructively interfere. This results in phase locking of the three discrete laser channels.

Fig. 16C exemplifies a resonator cavity **4000C**, configured generally similar to cavity **4000B**, but distinguishing therefrom in that three apertures of the previous example are replaced by a single large aperture **518**. In this case, no distinct light channels are formed, and continuously the field at each point is coupled to the fields at other points in the beam. This spatial coupling across the large beam introduced by a grating coupler **620** results in a single large coherent distribution with well defined amplitude and phase distribution. Thus, a large beam distribution with high power and potentially good beam quality can be obtained at the output.

Another problem solved by the present invention is associated with the fact that in a large-aperture multimode resonator cavity, the output power is high (large mode volume), but the beam quality is relatively poor (high M^2). The present invention provides for improving the beam quality of multimode laser resonators by modifying the resonator such that instead of using one highly multimode beam distribution in the gain medium, an array of Gaussian beam distributions is used, which beams are phase-locked and coherently added within the resonator, to obtain a single Gaussian output beam. As a result, the output power is lower than with the standard multimode configuration due to the fill factor of the Gaussian distributions, but the beam quality improves significantly. This conversion from a multimode beam distribution to a Gaussian distribution is done with relatively high efficiency.

Reference is made to **Figs. 17A and 17B** illustrating how an array of four Gaussian beam distributions replaces a corresponding multimode beam distribution.

Fig. 17A shows schematically a standard multimode resonator including a back mirror **12**, an output coupler **14**, and a gain medium **16** (laser rod) therebetween.

Fig. 17B shows a resonator configuration **5000** of the present invention including a back mirror **12**, an output coupler **14**, a gain medium **16** of the multimode resonator, a specially designed aperture arrangement **5018**, and a beam coupler assembly including two interferometric couplers **20A** and **20B**. In the

present example of **Fig. 17B**, the aperture arrangement **5018** is designed as a multiple-aperture configuration including four apertures, each with a diameter suitable for Gaussian mode operation. It should, however, be noted that a similar effect can be achieved by using a single rectangular-shaped aperture configuration (e.g., square aperture for the case of two pairs of beams). It should be understood that for a given resonator, i.e. length and mirror curvatures, the aperture size preferably corresponds to four tightly packed channels. One coupler **20A** is designed and oriented so that it combines one pair of horizontally displaced Gaussian distributions **A** and **B** with another pair of horizontally displaced Gaussian distributions **A'** and **B'**, resulting in two Gaussian distributions **C₁** and **C₂** (instead of four) that are horizontally displaced with respect to each other. The other coupler **20B** is oriented so that it combines these two Gaussian distributions **C₁** and **C₂** into one Gaussian distribution **C**. As indicated above, the laser will tend to operate in the minimal loss state, where all the beams phase lock and add up coherently, provided that there is at least one common longitudinal mode (frequency) for all four channels. This could be achieved by inserting additional optical elements into the channels to obtain the appropriate optical path lengths.

The multiple-aperture arrangement **5018** in the optical path of input beams may be replaced by a single aperture in the common path **C** as shown in the figure in dashed lines.

As indicated above, yet another option is to use a single square aperture in the optical path of input beams. In this case, the thickness of the interferometric plates **20A** and **20B** and the resonator mirrors **12** and **14** are appropriately designed such that four Gaussian or multimode beam distributions are "tightly packed" within the gain medium **16** and coherently added.

It should be understood that the configuration of **Fig. 17B** could be easily scaled to larger arrays by using additional pairs of interferometric plates. For example, for 16 Gaussian distributions (4x4 array) four interferometric couplers are used, and special care is taken to fulfill the common longitudinal mode requirement. Generally speaking, if the common frequency requirement is fulfilled, this scheme can be extended even further. It should also be noted that the example

of Fig. 17B, using an array of Gaussian beams and intra-cavity interferometric couplers, could be extended to other configurations where an array of low order multimode beam distributions and other types of couplers (as described above) are used. Considering the use of a single square aperture at the input beams path, and
5 4x4 array output, two pairs of interferometric plates with different thicknesses are used, where the thickness of the plates in the first pair is twice the thickness of the plates in the second pair.

A possible Nd:YAG laser experimental setup is shown in Fig. 18 and generally designated **6000**. The resonator is basically about 70cm long plano-
10 concave resonator, with a concave ($R = 3$ m) output coupler **14** of 40% reflectivity at 1064nm and a high-reflective flat mirror **12**. An (A) Nd:YAG rod **16** of 5mm diameter and 10cm length, with 1.1% doping, is placed in a diffusive ceramic pump chamber. The resonator includes a double aperture **18** with two apertures of 1.6 mm diameter each, positioned 2.4mm apart (between centers), and a high quality thin
15 film polarizer **30**. In general a polarizer is not needed, however in order to obtain high accuracy in the coatings transmission and to exploit Brewster angle instead of AR coating, a single polarization state is preferable. The 3mm thick interferometric coupler **20** is positioned at Brewster's angle. Half of its first (front) facet is coated with a 50% beam splitter coating **21A'**, and half of its second (rear) facet is coated
20 with a high reflective coating **21B'** (no AR coatings). An optional arrangement **32** comprised of an electro-optical LiNbO₃ crystal and a $\lambda/4$ retardation plate can be used for Q-switching. CCD cameras (near field camera and far field camera) **34A** and **34B** and Spiricon Laser Beam Analyzers are used for detecting and characterizing the near and far field intensity distributions.

25 Thus, the present invention provides novel resonator cavity configurations, as well as couplers to be used therein, for achieving intra-cavity phase locking, or phase locking and coherent addition, of two or more Gaussian beams, two or more single-high-order-transverse-mode beams, and two or more transverse multimode beams. The technique of present invention provides for imposing the modal
30 distribution content of one channel on all other channels within the laser resonator

cavity, and coherently combining all these distributions to obtain a single powerful beam at the output, with the desired modal content.

The technique of the present invention provides for designing compact, stable and practical laser systems whose outputs will have both high power and high beam quality, much above those from single channel high power lasers. The compactness of the single-substrate coupler enables the combined lasers to “share” optical components such as the end resonator mirrors. This further improves the stability of the combined system, as vibrational and thermal noises are largely common-mode-rejected. The flexibility to design and fabricate complex elements on a single substrate enables control of the coupling strength so as to optimize the trade off between coupling and loss (for high-gain lasers strong coupling between the lasers is required for phase locking, whereas for low-gain lasers weak coupling is better). In the technique of the present invention, external polarization manipulation can be used as an additional degree of control. Indeed, the use of orthogonal polarizations for two lasers will enable efficient addition even without interferometric stability. Slightly different wavelengths may also be used for the same purpose. The couplers can be designed to combine lasers operating with higher order modes, and even multimode beams, enabling even higher total powers than with lasers operating with the single fundamental mode. Single-substrate optical elements can be mass produced, and offer substantial savings in manufacturing, assembling and combining of many individual lasers.

The technique of the present invention can be applied to a wide variety of lasers (gas, solid state, diode, fiber, microdisk, etc), a variety of stable resonators, and various modes of operation (CW, pulsed, etc), which could be used in industrial, medical, and military applications.

Those skilled in the art will readily appreciate that various modifications and changes can be applied to the embodiments of the invention as hereinbefore described without departing from its scope defined in and by the appended claims.